# Darlington Power Transistors in Audio Amplifiers

EB 103

Price 20p

# **SUMMARY**

A description is given of three amplifiers with the following output powers:

- a) 75W from 2 x 32V rails into  $4\Omega$
- b) 50W from 2 x 26V rails into  $4\Omega$
- and c) 25W from 2 x 20V rails into  $4\Omega$

These audio circuits are designed primarily for mains powered home equipment.

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EB103

# DARLINGTON POWER TRANSISTORS IN AUDIO AMPLIFIERS

#### INTRODUCTION

The use of Darlington transistors in audio amplifiers gives the advantage of a lower component cost and thus mounting cost, both by reducing the number of actual devices required and, through their high gains, the number of conventional driver stages. Also by using complementary Darlington output stages the problem of providing inversion stages is removed.

### CIRCUIT DESCRIPTION

A circuit diagram of the 25 and 50W amplifier is given in Figure 1 and of the 75W amplifier in Figure 2. These amplifiers use direct coupling at the output and consequently a differential stage is used at the input to ensure low offset voltages. Otherwise, excessive offset could lead to de-centring of the loudspeaker cone or, in the extreme case, its destruction. Negative feedback is also provided to the

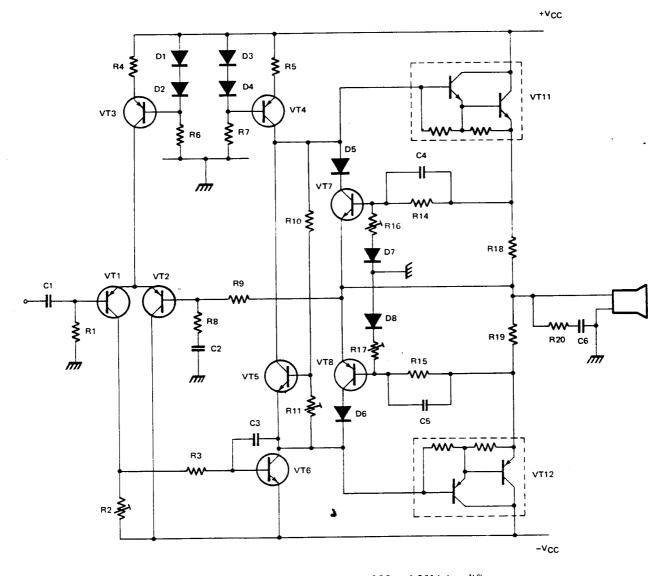


FIGURE 1. Circuit Diagram of 25 and 50W Amplifiers

differential stage, defined by resistors R8 and R9. Transistor VT1 of the pair also drives the class A driver stage comprising of transistor VT6. The latter has, between collector and base, a Miller capacitor in order to improve the high frequency stability. The use of a constant current supply (transistor VT4) gives a high mains supply ripple voltage rejection. It also means that a 'bootstrap' capacitor is not required and thus gives some space saving. The quiescent current is adjusted to 50mA by means of the trim potentiometer R11 in a VBE multiplier stage, transistor VT5. (Positioning the trim potentiometer here rather than in the resistor R10 position, means that should it go open circuit the output will be turned off rather than the catastrophic fully on). The use of Darlington power transistors as the output devices allows the design to deliver 50W without additional driver devices.

#### Temperature Compensation of the Quiescent Current

The first evaluation of a 25W audio amplifier, with TIP120/125 Darlington transistors, employing a BC183 silect transistor in the  $V_{BE}$  multiplier position, VT5,

showed the quiescent current to be heavily temperature dependent. At an ambient temperature of approximately 60°C thermal instability of the Darlington output stage starts to occur. Thus the poor thermal contact of the silect transistor means that it is necessary to use an SOT-32 transistor type in the VBE multiplier stage. To additionally reduce the thermal resistance it is suggested that a proprietary silicon grease is also used. With this, the temperature change of the quiescent current is completely compensated.

#### Construction

Due to the high current gains oscillation problems could occur in the amplifier if care is not taken with the construction. Through careful wiring and layout, oscillations can be avoided. Practice has shown that twisting the short leads to the output transistor, use of the VBE multiplier (with transistor VT5 attached to the heat sink) and adding a high frequency stabilising network (R20 and C6) across the load are all helpful. Also it is good practice to bring the ground lines to a star point near the supply source.

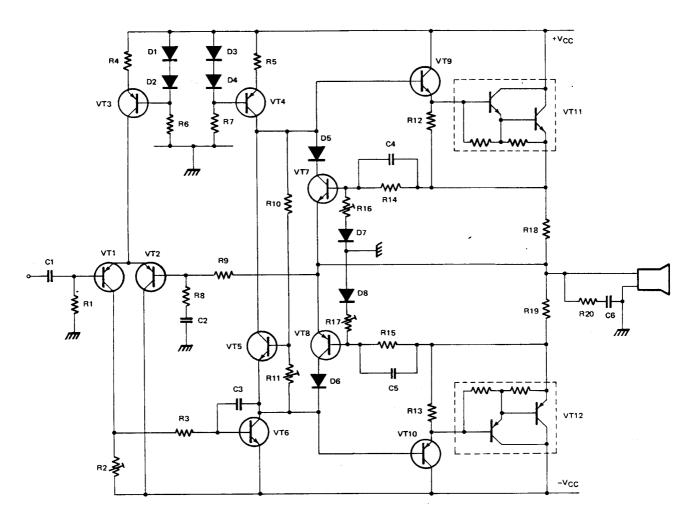


FIGURE 2. Circuit Diagram of 75W Amplifier

#### Components List

# **CALCULATIONS**

Componento sast					
	25W	50W	75 <b>W</b>	For the 25W into $4\Omega$ Amplifier	
R1	$120 \mathrm{k}\Omega$	$120 \mathrm{k}\Omega$	$120 k\Omega$		
R2	2k5	2k5	2k5	Specification $P_{out} = 25W$	
R3	1 k	1 k	1 k	R: - 40	
R4	560	560	560	$R_L = 4\Omega$	
R5	56	47	180	Input Impedance $R_{in} \ge 100 k\Omega$	
R6	3k3 ,	3k3	3k3	Voltage gain    40dB	
R7	3k3	3k3	3k3	• •	
R8	1k2	1 k2	1 k2	V <sub>in</sub> for full output 110mV	
<b>R</b> 9	110k	110k	11 <b>0</b> k		
R10	1 k8	1k8	3k3	Supply voltage $V_S = (P_{out} \times 8 \times [R_L + R_{in}])^{1/2}$	
R11	1 k	1 k	1k		
R12, R13	_	_	470	$+2 \times V_{CE(sat)}$	
R14, R15	270	270	270	$P_{out} = 1.2 \times P_{out} = 30W$	
R16, R17	5k	5k	5k		
R18, R19	0.27	0-27	0.27	RE is chosen to be $0.27\Omega$	
R20	$2\Omega7$	$2\Omega7$	$2\Omega7$	where $R_E = R18 = R19$	
C1	680nF	680nF	680nF	$R_L = 4\Omega$	
C2	47μF	47μF	47μF	$V_{CE(sat)} = 2V$	
C3	27pF	27pF	27pF	VCE(sat) = 2 V	
C4, C5	10nF	10nF	10nF	$\therefore V_S = (60 \times 8 [4 + 0.27])^{\frac{1}{2}} \times 2 \times 2$	
C4, C5	100nF	100nF	100nF	VS = (00 X 0 [4 + 0.27])	
Co	100111			= 36V	
D1-D6	1N914	1N914	1N914		
VT1-VT4	BC212	BC212	BC212	2 x 20V supplies would be quite adequate.	
VT1-V14 VT5	BC212 BC429	BC429	BC429	••	
	BC429 BC182	BC182	BC182	The peak collector current of the output transistors	
VT6-VT7 VT8	BC182 BC212	BC212	BC212	VT11 and VT12	
VT9		DC212 -	BC182	$\hat{I}_C = (V_S - 2 \times V_{CE(sat)})/2 \times R_L + R_{in})$	
	<del></del>	<del>-</del>	BC212	$IC = (VS - 2 \times VCE(sat))/2 \times RL + Rin)$	
VT10	- TIP120	_ TIP130	TIP141	1 D 00 D = 220	
VT11		TIP135	TIP146	where $R_L = 0.8 \times R_L = 3.2\Omega$	
VT12	TIP125	111133	111170	$\hat{1}_{C} = (40 - 2 \times 2)/2 \times (3.2 + 0.27) = 5.2A$	

In order to meet these requirements ( $V_{CEO} = 60V$  and  $I_{C} = 5A$ ) the correct Darlington transistors for the output devices are the TIP120 and TIP125.

$$I_B = I_C/h_{FE}$$
 where hFE = 1600  
 $I_B = 5/1600 = 3.12 \text{mA}$ 

With a resistor value of  $56\Omega$  for R5, the constant current value

$$I_q = 0.7/56 = 12.5 \text{mA}$$
  
and an output driving ratio  
$$V = I_B/I_q = 3.12/12.5 = 0.25$$

Graphs of total harmonic distortion (t.h.d.) versus output power and versus frequency for this amplifier are given in Figures 3 and 4, and the frequency response is shown in Figure 5.

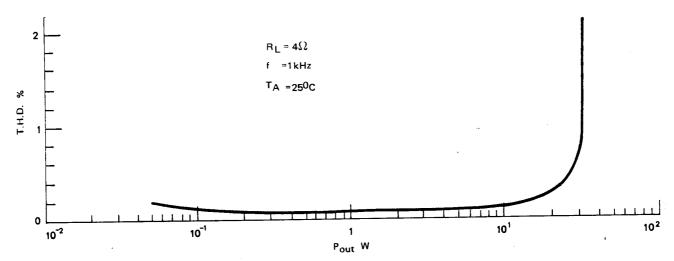


FIGURE 3. T.H.D. vs Output Power of 25W Amplifier

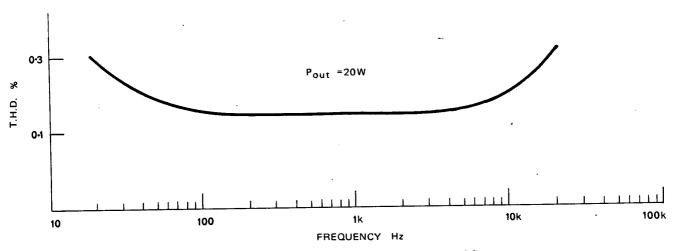


FIGURE 4. T.H.D vs Frequency of 25W Amplifier

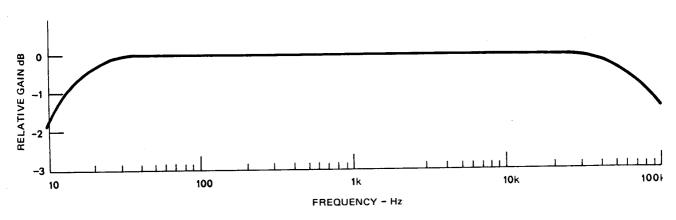


FIGURE 5. Frequency Response of 25W Amplifier

# 50W into $4\Omega$ Amplifier

Rest of Specification

Input Impedance  $R_{in} = 100k\Omega$ 

 $V_{in}$  for full output = 157mV

Suitable supply voltages are ±26V and Darlington

Transistors to supply the required 6.8A are the TIP130 and TIP135.

Graphs of t.h.d. versus output power and frequency, and frequency response for this amplifier are given in Figures 6, 7 and 8 respectively.

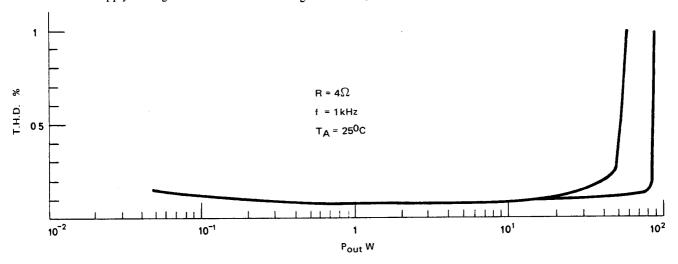


FIGURE 6. T.H.D. vs Output Power of 50W and 75W Amplifiers

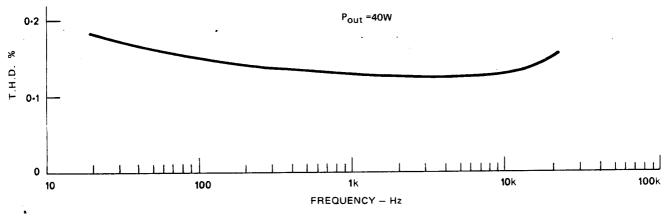


FIGURE 7. T.H.D. vs Frequency of 50W Amplifier

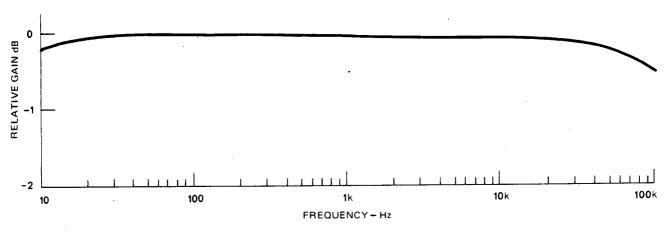


FIGURE 8. Frequency Response of 50W Amplifier

#### 75W into $4\Omega$ Amplifier

Rest of Specification

Input Impedance  $R_{in} = 100k\Omega$ 

 $V_{in}$  for full output = 192mV

Suitable supply voltages are ±31V and Darlington transistors to supply the required 8.2A are the TIP141 and TIP146.

The use of a constant current source giving approximately 20mA is not possible due to the high power requirements for transistors VT4 and VT5. Therefore in order to have relatively small currents and minimum power dissipation in the class A driver and the constant current supply device, small signal driver transistors are employed.

Graphs of t.h.d. versus output power and frequency, and frequency response are given in Figures 6, 9 and 10 respectively.

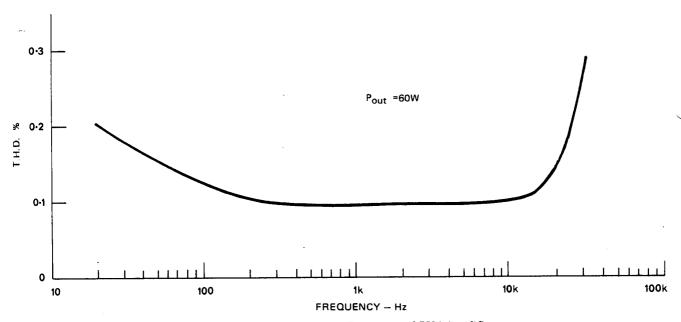


FIGURE 9. T.H.D. vs Frequency of 75W Amplifier

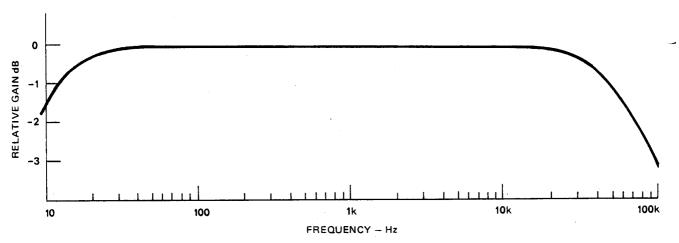


FIGURE 10. Frequency Response of 75W Amplifier